

METHOD FOR FINDING THE REFLECTIVITY OF REFLECTORS

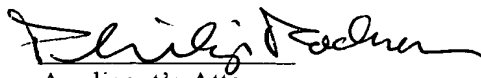
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Introduction

The ultimate goal of seismics is to find the physical properties of the subsurface. Seismic energy in the form of compressional or shear waves are transmitted into the ground and the reflections (echoes) from structures in the subsurface are recorded by sensors
 5 (hydrophones or geophones) most commonly located at, or near the surface of the earth.

The wave field recorded by the sensors is then processed in computers. The resulting "sound images" of the subsurface are interpreted by geophysicists and geologists to make maps of the structures. These structures are mainly represented by interfaces separating layers with different physical properties. These interfaces are detectable only because they are capable of reflecting seismic energy.
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This patent application describes a new method that estimates the reflectivity, expressed by the angle-dependant reflection coefficient, from seismic measurements.

15 There is a comprehensive literature on methods for estimating the reflectivity of reflectors in the subsurface. Such methods are often called "True Amplitude Migration (TAM)" methods. Within the scope of this patent application it is not possible to give a full review of all methods published, but a common feature of the existing methods is
 20 that they estimate both the spatial position and its reflectivity in one operation.

A review and comparison between several existing methods is found in [1] in the list of references. Important publications within TAM are [2], [3], [4], [5], [6] and [7].

25 Figure captions

The characteristics of the invention described of this patent application are explained with the aid of a series of figures where:

figure 1 : In Kirchhoff prestack depth migration, the recorded trace for shot/receiver pair # i is stacked into position \bar{x} in depth. In this case there are 4 ray paths that are
 30 candidates to a reflected pulse in the receiver. The ray paths are A-1 (ray A from Shot to position \bar{x} and ray 2 from \bar{x} to Receiver), and correspondingly, A-2, B-1 and B-2. Usually, only one of these ray paths will be used in the migration. On the figure, the isochrones (i.e surfaces of constant travelttime between Shot-isochrone-Receiver) corresponding to two of the 4 possible ray paths are shown. The points

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where these isochrones are tangent to the (unknown) reflectors, will be reflection points of the rays from shot to receiver. In this case, there are two rays with traveltimes $t_{i2}(\bar{x})$ and $t_{i4}(\bar{x})$ that reflects in depth point \bar{x} .

figure 2 : In Kirchhoff prestack depth migration, the reflected pulse for shot/receiver pair (# i) is stacked in all points in-between the two isochrones τ_n and $\tau_n + T$ in depth. Along a band of width L at the reflector, there will be constructive interference between all the N pulses that are stacked to depth. If we call the set of depth points within this band \bar{x}_L , it is necessary to stack only the points in-between the two isochrones for which $\bar{x} = \bar{x}_L$.

figure 3 : The modelled pulse # n for shot/receiver pair # i is stacked in stacking stick # j . A stacking stick is a curve parametrized by ξ_j and crossing the reflector with parametric value $\xi_j = 0$. ξ_{jk} is a discrete value of ξ_j along the stacking stick. Only one stacking stick is shown in full length. The others are indicated as short vertical ticks along target reflector. The stacking sticks are located at the boundaries of the reflector segments of area ΔT_p .

figure 4 : Target reflector (in birds eye perspective) is parametrized by a triangular network. The Reflection Coefficient (RC) in stacking stick # j are found from rays with reflection points marked by black dots. The RC on the target reflector is parameterized by constant RC, R_p^T , in each of the P triangles of the network.

figure 5 : A two-layer model with a syncline in the interface between $x=4$ km and $x=8$ km. In the upper layer, the seismic velocity of the P-waves (i.e. compressional waves) is 4.0 km/s, the velocity of the S-waves (i.e. the share waves) is 2.28 km/s and the density is 2.0 g/cm³. In the lowermost layer, the velocity and density is specified in the figure. The rays from shot # 100 to the receivers are also shown.

figure 6 : A seismic depth section from PSDM of the lowest offset interval (shot/receiver distance from 25 m to 300 m) using the seismic data generated in the model shown in figure 5.

figure 7 : Maximum amplitude (i.e. peak amplitude) along target reflector in the seismic depth section in figure 6 superimposed on the real reflection coefficient.

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figure 8 : Real and estimated (by ROAR) angle dependant reflection coefficient in position **A** ($x=3$ km) and **B** ($x=5$ km) in the model.

figure 9 : Real and estimated (by ROAR) angle dependant RC for reflection angle close to 0 degrees along target reflector in the model in figure 5. Two of the weight functions (W_1 and W_2) giving the resolution in the estimated RC at point **C** and **D** are shown at the top of the figure.

Pre Stack Depth Migration (PSDM)

10 In order to describe the new method of this patent application, we start with a description of Kirchhoff pre stack depth migration (references [5], [6], [7]), often abbreviated to PSDM (Pre Stack Depth Migration). Consider figure 1 showing an unknown reflector, a generally variable velocity field $v(x,y,z)$ and a shot/receiver pair with a corresponding recorded time trace. A seismic *survey* often consists of millions of
 15 shot/receiver pairs. Note that we consider a 3-dimensional (3-D) volume even though the illustrations are shown in 2-D for simplicity. We now assume that PSDM is used to move (i.e. to migrate) the recorded data from the receivers at the surface down to a general position \vec{x} in the subsurface. Such a depth migration is generally described by the equation

$$20 \quad P_{Obs}(\vec{x}) = \sum_{i=1}^I \sum_{j=1}^{J(i)} w_{ij}[\vec{x}] \cdot \dot{p}_i[t_{ij}(\vec{x})] \quad (1)$$

where I is the number of traces that are stacked in a general position \vec{x} in the subsurface,

$t_{ij}(\vec{x})$ is traveltime # j of the $J(i)$ possible ray paths from the shot via \vec{x} to the receiver for shot/receiver pair # i

25 $\dot{p}_i[t_{ij}(\vec{x})]$ is the time derivative of the i 'th time trace evaluated in time $t_{ij}(\vec{x})$, and
 $w_{ij}[\vec{x}]$ is the weight on the trace value $\dot{p}_i[t_{ij}(\vec{x})]$.

The unknown quantities at the right of equation 1, $t_{ij}(\vec{x})$, $J(i)$ and $w_{ij}[\vec{x}]$ are generally computed by ray modeling (as described in references [8], [9], [10]), or by finite difference solution of the Eikonal equation as described in references [13] and [14].
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When a large number of traces are stacked as described in equation 1, the reflected pulses from the unknown reflector is migrated into depth along isochrones (i.e. surfaces of constant traveltime shot-isochrone-receiver) that are tangential to the unknown reflector. This will lead to constructive interference along the reflector and destructive interference away from the reflector. Hence the migrated seismic cube, $P_{Obs}(\vec{x})$, shows higher amplitudes on and near the reflector so that the position of the reflector may be determined.

In the development of TAM within PSDM, great effort has been spent in deriving formulas for calculating weights $w_i[\vec{x}]$ giving amplitudes in $P_{Obs}(\vec{x})$ that are proportional with the Reflection Coefficient (RC) along the reflectors in the depth model (see references [2], [5], [6] and [7]). The definition of the reflection coefficient as described in reference [11] is the ratio between the amplitude of an incidence plane wave field and its reflected plane wave field from a plane reflector.

In addition, there has been done much work in finding which of the $J(i)$ possible ray paths from shot via the depth point \vec{x} to the receiver that gives the best result in the migration. An accepted criterion for finding this "best" ray path is to use the ray from shot/receiver pair to \vec{x} having the *highest amplitude* as described in reference [12]. Lately, also the rays with the *shortest ray path* have been used with good results. By selecting only one of the $J(i)$ possible ray paths between shot-x-receiver, equation 1 may be simplified to

$$P_{Obs}(\vec{x}) = \sum_{i=1}^J w_i[\vec{x}] \cdot \dot{p}_i[t_i(\vec{x})] \quad (2)$$

where $t_i(\vec{x})$ is the traveltime of the selected ray path from shot via \vec{x} to the receiver for shot/receiver pair # i ,
 $\dot{p}_i[t_i(\vec{x})]$ is the time derivative of the i 'th trace $p_i[t]$ for traveltime $t = t_i(\vec{x})$,
and $w_i[\vec{x}]$ is the weight on the trace value $\dot{p}_i[t_i(\vec{x})]$.

In the description of the new method below we assume constant, unit weights, i.e. that $w_i[\vec{x}]$ is 1.0 for all \vec{x} and i .

Description of the new method

The method described in this patent application is called "Reflector Oriented Amplitude Correction", abbreviated to ROAR.

5 Essence of ROAR

The starting point (what is assumed known) is:

- A seismic *survey*, i.e. the positions of all shots and receivers in a seismic acquisition.
- Characteristic properties of shot and receivers such as source pulse, directionality,
10 and filter properties.
- Pre-stack depth migrated *constant-offset* or *constant-angle* seismic data cubes.
- Position and shape of the "*target reflector*" for which the reflection coefficient is to be estimated.
- Model parameters (i.e. seismic velocities, densities, anelastic damping factors, interfaces etc.) of the part of the model lying above the target reflector.
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The results are:

- Discrete estimates of the angle dependant reflection coefficient for all illuminated areas of the target reflector. (equation 25 and 31).
- A weight function (equation 47) for all discrete estimates of the reflection coefficient along the target reflector.
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The advantages are:

- Explicit use of the reflector so that better estimates of RC may be achieved.
- Discrete estimates of RC for all illuminated areas of the surface with associated reflection angles.
- A weight function for all estimates of RC giving the resolution of the estimates along the target horizon.
- The possibility of finding the RC in models with acoustic as well as elastic materials.
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- The possibilities of including different wave modes to estimate the RC's for PP-, PS-, SP- and SS-reflections.
- The possibility of using multiples for estimating the RC's along the target horizon.
- A better treatment of the limited extension of the seismic survey and holes and missing traces in the data.
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- A possibility to improve the estimate of the RC's by including more complete ray modeling based on e.g. anisotropic ray theory and/or anelastic damping.

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- As mentioned above, most of the existing TAM methods try to solve the problem by finding both the reflector position and its reflection coefficient (RC) in one single process by using PSDM with weights on the trace samples that are migrated to depth. As opposed to this, ROAR estimates the reflector position and its RC in a process consisting of five steps. Steps 1, 2 and 3 are known techniques, while steps 4 and 5 are the essence of the invention:

- 10 **Step 1:** The recorded traces are migrated by PSDM by equation 1. When ROAR is to be used, it is an advantage, but not a necessity, to use the simplest and fastest version of PSDM with unit weights (i.e. with weights=1.0). The result of this process is a depth migrated seismic cube, $P_{Obs}(\vec{x})$.
- 15 **Step 2:** $P_{Obs}(\vec{x})$ is *interpreted* so that the spatial positions of the reflectors in the subsurface are found. Based on these reflectors and the seismic velocities (the velocities used in the PSDM in step 1) a depth model is constructed in the computer. One of the surfaces in the model is chosen as a target reflector.
- 20 **Step 3:** By modeling based on ray tracing, the reflected pulses from the target reflector for all shot/receiver pairs are estimated. Since we simulate the seismics in a depth model in the computer, we are free to select any value of the RC at the target reflector. In ROAR we are setting the RC to 1.0 for all reflection points and for all reflection angles along the target reflector. This means that *all* energy will be reflected from the target reflector.
- 25 **Step 4:** By doing a local PSDM on the synthetic, ray-tracing based traces from step 3 in a band around the target reflector, we will get a modeled, synthetic PSDM result, $P_{Mod}(\vec{x})$, locally around target reflector. The weight (see equation 1) used in this local PSDM must be identical to the weight used in the “real” PSDM in step 1.
- 30 **Step 5:** Measurements of the amplitudes along the target reflector from the real, depth migrated cube $P_{Obs}(\vec{x})$ is divided by corresponding measurements from the modeled PSDM, $P_{Mod}(\vec{x})$. The amplitude measurements may

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where τ_k is the traveltime of the ray,

$s(t)$ and $h(t)$ are the source pulse and its Hilbert transform,

$$\left. \begin{array}{l} s(t) \\ h(t) \end{array} \right\} \begin{array}{l} \neq 0 \quad t \in [0, T] \\ = 0 \quad t \notin [0, T] \end{array}, \quad \text{where } T \text{ is the duration of the source pulse,}$$

$R_k = R_k(\phi_k)$ is the unknown, complex, angle dependent RC for the ray in reflection point \vec{R} on the target reflector for reflection angle ϕ_k (see figure 3),

and Q_k is a complex number giving the combined effect of geometrical spreading, transmission and/or reflection loss by other reflectors (than target reflector), phase shift caused by focal points (also called caustics) and anelastic damping.

Ray modeling may compute many parameters along the ray path. In addition to the reflection point \vec{R} , the parameters:

- ray tangent vector for the incidence ray in \vec{R} ,
- ray tangent vector for the departing ray from \vec{R} ,
- ray tangent vector for the departing ray from the shot point,
- ray tangent vector for the incidence ray to the receiver point

and more may be computed. The use of these parameters will be discussed below.

As mentioned above, each of the I traces that are added into the depth point \vec{x} in equation 2 may be estimated by ray modeling

$$\dot{p}_i[t_i(\vec{x})] = \sum_{k=1}^{P(i)} \dot{g}_k[t_i(\vec{x})] \quad (4)$$

where $P(i)$ is the number of rays between shot/receiver number i .

We then insert equation 4 into equation 2 and assume that the weight $w_i[\vec{x}]$ is 1.0 and we get

$$P_{Obs}[\vec{x}] = \sum_{i=1}^I \sum_{k=1}^{P(i)} \dot{g}_k[t_i(\vec{x})] \quad (5)$$

We know that there has been a constructive interference between the migrated pulses along the target reflector. Therefore it is not necessary to stack traces for values of \vec{x} that are outside a certain distance from target reflector. This will reduce the number of pulses \dot{g}_k that needs to be stacked in equation 5 since the pulses have a limited duration. Assuming that \vec{x} lies within a band centered at the target reflector as shown in figure 2, equation 5 may be expressed as

$$P_{Obs}[\vec{x}] = \sum_{n=1}^N \dot{g}_n[t_n(\vec{x})] \quad \vec{x} \in \vec{x}_L \quad (6)$$

where

\vec{x}_L is the set of all positions within the band around target reflector

and

N is the number of ray-based pulses g_n in equation 5 characterized by the following property:

$$\tau_n < \tau_n(\bar{x}) < \tau_n + T \quad \bar{x} \in \bar{x}_L \quad (7)$$

- 5 where T is the duration the pulse, as shown in figure 2. The pulse corresponding to the ray path between the shot/receiver pair in figure 2 is mapped into point \bar{x} since \bar{x} is within the band around the reflector, i.e. $\bar{x} \in \bar{x}_L$.

We introduce a new definition, a *Stacking Stick*.

- 10 **Definition:** A *Stacking Stick* is a curve with a certain length L_ξ crossing target reflector as illustrated in figure 3 where stacking stick # j is shown in full length. The length L_ξ gives the width of the band around target reflector. L_ξ is chosen so large that it covers a few dominant wavelengths of $P_{Obs}(\bar{x})$ around target reflector. A stacking stick is parameterized by
- 15 $\bar{x}_j(\xi_j)$ giving the spatial position. The argument ξ_j starts with the value $\xi_j = \xi_{jA}$ in one end of the stacking stick, passes $\xi_j = 0$ at the intersection between the stacking stick and target horizon and ends in $\xi_j = \xi_{jB}$ in the other end of the stacking stick.

- 20 In figure 3 the stacking sticks are shown as vertical line segments crossing the Target Reflector, but the stacking sticks may also be chosen perpendicular to the target reflector. $P_{Obs}(\bar{x})$ is usually sampled on a regular, 3-dimensional Cartesian network (also called a *seismic cube*) with the discrete spatial positions given by

$$\bar{x}_{ijk} = \bar{x}_0 + \langle (i-1)dx, (j-1)dy, (k-1)dz \rangle \quad (8)$$

- 25 where \bar{x}_0 is the position to the lower corner of the cube and (dx, dy, dz) are the increments between the cube positions in x -, y - and z direction respectively. In order to find values of $P_{Obs}(\bar{x})$ in stacking stick # j , interpolation (linear or higher order) is used to find $P_{Obs}[\bar{x}_j(\xi_j)]$.

- 30 Assume that \bar{x} in equation 6 is located on a particular stacking stick (# j) with spatial position. $\bar{x}_j(\xi_j)$. For simplicity we express the observed trace in stacking stick # j by

$$P_{Obs}(\xi_j) = P_{Obs}[x_j(\xi_j)] \quad (9)$$

- The same simplification may be used in the expression for the Kirchhoff traveltime
- 35 from shot $\rightarrow \bar{x} \rightarrow$ receiver when \bar{x} is located on a stacking stick, i.e. that $\bar{x} = \bar{x}_j(\xi_j)$.

$$t_n(\xi_j) = t_n[x_j(\xi_j)] \quad (10)$$

Then we introduce $t'_n(\xi_j)$, an approximation to the Kirchhoff traveltime $t_n(\xi_j)$ in equation 6. The approximation $t'_n(\xi_j)$ use so called paraxial extrapolation [8] of the travel time values around the reflection point \bar{R} (see figure 3) for ray path # n from shot via $x_j(\xi_j)$ on the stacking stick # j to the receiver. Paraxial extrapolation means that

$$t'_n(\xi_j) \approx t_n(\xi_j) \quad (11)$$

for stacking sticks in the neighborhood of \bar{R} . By using this approximation, $g_n[t_n(\xi_j)]$

from equation 3 and equation 6 can be reformulated to

$$g_n[t'_n(\xi_j)] = \text{Re}\{R_n(\varphi_n)Q_n\}s(t'_n(\xi_j) - \tau_n) - \text{Im}\{R_n(\varphi_n)Q_n\}h(t'_n(\xi_j) - \tau_n) \quad (12)$$

Since the reflection angle, φ_n , is included in equation 12, we can introduce the angle dependency in $P_{obs}(\xi_j)$ and write equation 6 as

$$P_{obs}(\xi_j, \tilde{\varphi}_j) = \sum_{n=1}^N \left\{ \text{Re}\{R_n(\varphi_n)Q_n\}s(t'_n(\xi_j) - \tau_n) - \text{Im}\{R_n(\varphi_n)Q_n\}h(t'_n(\xi_j) - \tau_n) \right\} \quad (13)$$

where $\tilde{\varphi}_j$ is a weighted mean of the N reflection angles φ_n in equation 13. A closer definition of this angle will be presented later.

Furthermore, we assume a *real* RC, $R_n(\varphi_n)$, as in e.g. PP reflection at sub-critical angle. We use this assumption in equation 13 to get

$$P_{obs}(\xi_j, \tilde{\varphi}_j) = \sum_{n=1}^N R_n(\varphi_n)P_n(\xi_j) \quad (14)$$

where

$$P_n(\xi_j) = \text{Re}\{Q_n\}s(t'_n(\xi_j) - \tau_n) - \text{Im}\{Q_n\}h(t'_n(\xi_j) - \tau_n) \quad (15)$$

Then we introduce a mean RC, $\tilde{R}(\xi_j, \tilde{\varphi}_n)$

$$P_{obs}(\xi_j, \tilde{\varphi}_n) = \tilde{R}(\xi_j, \tilde{\varphi}_n) \sum_{n=1}^N P_n(\xi_j) \quad (16)$$

where $\tilde{R}(\xi_j, \tilde{\varphi}_n)$ may be found by combining equation 14 with equation 16:

$$\tilde{R}(\xi_j, \tilde{\varphi}_n) = \sum_{n=1}^N w_n(\xi_j)R_n(\varphi_n) \quad (17)$$

with weights, $w_n(\xi_j)$, given by

$$w_n(\xi_j) = \frac{P_n(\xi_j)}{\sum_{i=1}^N P_i(\xi_j)} \quad (18)$$

Expression for PSDM of seismics from ray modeling

Above we found a ray tracing based approximation to PSDM of the observed (or measured) seismics, as presented in equation 16 for a band of width L_ξ along the target reflector. We will now find the corresponding expression for ray modeled traces in stacking stick # j in a model where target reflector with a RC set to 1.0 for all points and all angles, but with a shape identical to the target reflector in the real model. By the same reasoning as for the deduction of equation 6 we get:

$$P_{Mod}(\xi_j) = \sum_{n=1}^N \dot{g}'_n[t'_n(\xi_j)] \quad (19)$$

where

$t'_n(\xi_j)$ is the Kirchhoff travelt ime approximated by paraxial extrapolation [8] in the neighborhood of \bar{R} (see figure 3) for ray path # n from shot, via $\bar{x}_j(\xi_j)$ on stacking stick # j to receiver,

$\dot{g}'_n[t'_n(\xi_j)]$ is the time derivative of the n 'th ray modeled trace $g_n[t'_n(\xi_j)]$ obtained by setting $R_k=1.0$ in equation 3:

$$g'_n[t'_n(\xi_j)] = \text{Re}\{Q_k\}s(t'_n - \tau_k) - \text{Im}\{Q_k\}h(t'_n - \tau_k) \quad (20)$$

By comparing equation 20 with equation 15 we see that

$$\dot{g}'_n[t'_n(\xi_j)] = P_n(\xi_j) \quad (21)$$

which is inserted into equation 19 to get

$$P_{Mod}(\xi_j) = \sum_{n=1}^N P_n(\xi_j) \quad (22)$$

Equation 22 is the expression for the ray-modeled result of unweighted PSDM in a model where RC is 1.0 along target reflector. The number of rays, N , is the subset of all rays between all shot/receiver pairs with the property

$$\tau_n < t_n(\xi_j) < \tau_n + T \quad (23)$$

for at least one of the points $\bar{x}_j(\xi_j)$ on stacking stick # j .

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Estimation of reflection coefficient (RC), Square method

Based on equation 16 and equation 17 it can be shown that the following equation that involves *square* values of $P_{Obs}(\xi_j, \tilde{\varphi}_j)$ and $P_{Mod}(\xi_j)$ is an estimate of the square of the angle dependent RC in the intersection between stacking stick # j and the target reflector,

$$[\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2 = \frac{\int_{\xi_{jA}}^{\xi_{jB}} \{P_{Obs}(\xi_j, \tilde{\varphi}_j)F(\xi_j)\}^2 d\xi_j}{\int_{\xi_{jA}}^{\xi_{jB}} \{P_{Mod}(\xi_j)F(\xi_j)\}^2 d\xi_j} \quad (24)$$

where

$\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)$ is the estimate of the RC for the intersection point between stacking

stick # j and the target reflector for reflection angle $\tilde{\varphi}_j$,

$P_{Obs}(\xi_j, \tilde{\varphi}_j)$ is the observed, real PSDM trace in stacking stick # j ,

$P_{Mod}(\xi_j)$ is the ray modeled PSDM trace in stacking stick # j ,

$F(\xi_j)$ is a weight function along stacking stick # j and

(ξ_{j1}, ξ_{jK}) are the minimal and maximal value of ξ_j along stacking stick # j .

The discrete version of equation 24 is as follows.

$$[\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2 = \frac{E_{Obs}}{E_{Mod}} \quad (25)$$

where

$$E_{Mod} = \sum_{k=1}^K \{P_{Mod}(\xi_{jk})F(\xi_{jk})\}^2 \Delta\xi \quad (26)$$

and

$$E_{Obs} = \sum_{k=1}^K \{P_{Obs}(\xi_{jk}, \tilde{\varphi}_j)F(\xi_{jk})\}^2 \Delta\xi \quad (27)$$

where

ξ_{jk} is a discrete value of ξ_j with a corresponding position $\bar{x}_j(\xi_{jk})$ on stacking stick # j ,

and $\Delta\xi$ is the constant increment between the discrete positions

$\{\bar{x}_j(\xi_{jk}), \bar{x}_j(\xi_{j(k+1)}), \bar{x}_j(\xi_{j(k+2)}), \dots\}$ along stacking stick # j .

Inserting equation 22 into equation 26 and equation 16 into equation 27, it is also possible to derive a weight function for the contribution from the individual RC's in the neighborhood of stacking stick # j . The squared estimate of the RC may be expressed

as

$$[\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2 = \sum_{n=1}^N \tilde{W}_n(\xi_j, \tilde{\varphi}_j) R_n(\varphi_n) \quad (28)$$

where the weight, $\tilde{W}_n(\xi_j, \tilde{\varphi}_j)$, on the RC, $R_n(\varphi_n)$, in the reflection point \tilde{R} of ray # n is given by

$$\tilde{W}_n(\xi_j, \tilde{\varphi}_j) = \frac{\Delta \xi}{E_{Mod}} \sum_{k=1}^K F(\xi_{jk})^2 P_{Obs}(\xi_{jk}, \tilde{\varphi}_j) P_n(\xi_{jk}) \quad (29)$$

E_{Mod} is given by equation 26 and the depth migrated pulse $P_n(\xi_{jk})$ is found by ray modeling and equation 15. $P_n(\xi_{jk})$ is found from a ray with reflection angle φ_n as shown in figure 3.

Estimation of reflection coefficient (RC), Norm method

Based on equation 16 and equation 17 it can be shown that the following equation that involves *absolute* values of $P_{Obs}(\xi_j, \tilde{\varphi}_j)$ and $P_{Mod}(\xi_j)$ is an estimate of the absolute value of the angle dependent RC in the intersection between stacking stick # j and the target reflector,

$$|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| = \frac{\int_{\xi_{jA}}^{\xi_{jB}} |P_{Obs}(\xi_j, \tilde{\varphi}_j) F(\xi_j)| d\xi_j}{\int_{\xi_{jA}}^{\xi_{jB}} |P_{Mod}(\xi_j) F(\xi_j)| d\xi_j} \quad (30)$$

where

$\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)$ is the estimate of the RC for the intersection point between stacking stick # j and the target reflector for reflection angle $\tilde{\varphi}_j$,

$P_{Obs}(\xi_j, \tilde{\varphi}_j)$ is the observed, real PSDM trace in stacking stick # j ,

$P_{Mod}(\xi_j)$ is the ray modeled PSDM trace in stacking stick # j ,

$F(\xi_j)$ is a weight function along stacking stick # j and

(ξ_{j1}, ξ_{jK}) are the minimal and maximal values of ξ_j along stacking stick # j .

The discrete version of equation 30 is as follows:

$$|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| = \frac{N_{Obs}}{N_{Mod}} \quad (31)$$

where

$$N_{Mod} = \sum_{k=1}^K |P_{Mod}(\xi_{jk}) F(\xi_{jk})| \Delta \xi \quad (32)$$

and

$$N_{Obs} = \sum_{k=1}^K |P_{Obs}(\xi_{jk}, \tilde{\varphi}_j) F(\xi_{jk})| \Delta \xi \quad (33)$$

where

ξ_{jk} is a discrete value of ξ_j with a corresponding position $\bar{x}_j(\xi_{jk})$ on stacking stick # j ,

and $\Delta\xi$ is the increment between the discrete positions $\{\bar{x}_j(\xi_{jk}), \bar{x}_j(\xi_{j(k+1)}), \bar{x}_j(\xi_{j(k+2)}), \dots\}$ along stacking stick # j .

Inserting equation 22 into equation 32 and equation 16 into equation 33, it is also possible to derive a weight function for the contribution from the individual RC's in the neighborhood of stacking stick # j . The absolute value of the estimate of the RC may be expressed as

$$|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| = \sum_{n=1}^N \hat{W}_n(\xi_j, \tilde{\varphi}_j) R_n(\varphi_n) \quad (34)$$

where the weight, $\hat{W}_n(\xi_j, \tilde{\varphi}_j)$, on the RC, $R_n(\varphi_n)$, in the reflection point \bar{R} of ray # n is given by

$$\hat{W}_n(\xi_j, \tilde{\varphi}_j) = \frac{\Delta\xi}{N_{Mod}} \sum_{k=1}^K |F(\xi_{jk})| \text{sgn}\{P_{Obs}(\xi_{jk}, \tilde{\varphi}_j)\} P_n(\xi_{jk}) \quad (35)$$

N_{Mod} is given by equation 32 and the depth migrated pulse $P_n(\xi_{jk})$ is found by ray modeling and equation 15. $P_n(\xi_{jk})$ is found from a ray with reflection angle φ_n as shown in figure 3.

Weights and reflection angles

Two methods within ROAR have been used to estimate the angle dependant RC for a target reflector. The two methods are "square method" (equation 25)

$$[\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)]^2 = \frac{E_{Obs}}{E_{Mod}} \quad (36)$$

and "norm method" (equation 31))

$$|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| = \frac{N_{Obs}}{N_{Mod}} \quad (37)$$

It is shown above in equation 28 and 34, that the estimated RC's $[\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2$ and $|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)|$ may be expressed as weighted means of the RC's in the N reflection points in the neighborhood of stacking stick # j .

The weighted mean for the estimation of the RC in stacking stick # j using the square method is according to equation 28

$$[\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2 = \sum_{n=1}^N \tilde{W}_n(\xi_j, \tilde{\varphi}_j) R_n(\varphi_n) \quad (38)$$

and correspondingly for the norm method (equation 34)

$$|\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| = \sum_{n=1}^N \tilde{W}_n(\xi_j, \tilde{\varphi}_j) R_n(\varphi_n) \quad (39)$$

The equations for the weights in each of these methods are given in equation 29 and 35 respectively. Each of the N contributions in equation 38 and 39 corresponds to a particular ray with reflection point \vec{R} and a reflection coefficient (RC) equal to $R_n(\varphi_n)$ in the neighborhood of stacking stick # j . All the RC's in the neighborhood of stacking stick # j contributes to \mathfrak{R} , the estimate of the RC. This means that weights in equation 38 and 39 gives the *resolution* in the estimate of the RC.

We now assume that the target reflector is parameterized by a triangular network as shown in figure 4. In each node in the network there is a stacking stick. It is assumed that the real RC is constant in each of the P triangles that make up the network. The constant value of the RC in each of the P triangles is $R_1^T, R_2^T, R_3^T, \dots, R_P^T$. To each of the RC's it is associated a reflection angle $\varphi_1^T, \varphi_2^T, \varphi_3^T, \dots, \varphi_P^T$ which will be defined below.

Then equation 38 and 39 is expressed in the general form

$$b = \sum_{n=1}^N a_n R_n(\varphi_n) \quad (40)$$

where

$$b = [\mathfrak{R}_E(\xi_j = 0, \tilde{\varphi}_j)]^2 \quad ; \quad a_n = \tilde{W}_n(\xi_j, \tilde{\varphi}_j)$$

for the Square method, and

$$b = |\mathfrak{R}_N(\xi_j = 0, \tilde{\varphi}_j)| \quad ; \quad a_n = \tilde{W}_n(\xi_j, \tilde{\varphi}_j)$$

for the Norm method

Each of the discrete values $R_n(\varphi_n)$ of the RC in equation 40 corresponds to a reflection point in figure 4.

Next we define to subsets:

S_p : the subset of the N reflection points in equation 40 located in triangle # p .

S^T : the subset of all the P triangles in target horizon that contains at least one of the N reflection points in equation 40.

Using this, the relation between $R_n(\varphi_n)$ and R_p^T may be expressed as

$$R_n(\varphi_n) = R_p^T \quad (41)$$

for all $R_n(\varphi_n)$ with reflection points in the subset S_p , that is for all $n \in S_p$.

The reflection angle ϕ_p^T associated to R_p^T is defined as

$$\phi_p^T = \frac{\sum_{n \in S_p} \phi_n}{\# \text{elements in } S_p} \quad (42)$$

By using equation 41 in equation 40, the latter equation may be expressed as

$$b = \sum_{p \in S^T} A'_p R_p^T \quad (43)$$

where

$$A'_p = \sum_{n \in S_p} a_n \quad (44)$$

In order to find a weight function that gives the weight “per unit area” of the target reflector we consider a continuous weight function $A(\vec{x}_s)$ with this property. Such a weight function would have to be integrated over the target reflector with a continuous RC function $R^T(\vec{x}_s)$ in the following way.

$$b = \int_S A(\vec{x}_s) R^T(\vec{x}_s) dS \quad \text{where } S \text{ is Target Reflector} \quad (45)$$

This equation may be parameterized in the following way using the triangular parameterization of the target reflector described above and shown in figure 4.

$$b = \sum_{p \in S^T} A_p R_p^T \Delta T_p \quad (46)$$

In this equation, ΔT_p is the area of triangle # p while

A_p and R_p^T are the weight and RC respectively, associated to triangle # p .

By comparing equation 46 with equation 43, we see that the discrete approximation to a “per unit area” weight function is

$$A_p = \frac{A'_p}{\Delta T_p} = \frac{\sum_{n \in S_p} a_n}{\Delta T_p} \quad (47)$$

giving the weight per unit area for the RC in triangle # p in the subset S^T .

The reflection angle $\tilde{\phi}_j$ associated to the estimate of b (i.e. the estimation of the RC as shown in equation 40) is found by a weighted mean of the angles ϕ_p^T from equation 42

$$\tilde{\phi}_j = \sum_{p \in S^T} W_p^T \phi_p^T \quad (48)$$

with weights

$$W_p^T = \frac{|A'_p|}{\sum_{k \in S^T} A'_k} \quad (49)$$

where A'_p is given by equation 44.

5 Example

As an example of the application of the new invention, the simple 2-D (two dimensional) model shown in figure 5 is used. The model consists of two layers separated by a target reflector with a syncline of depth 1 km between $x=4$ km and $x=8$ km. The lower layer consists of 5 zones with constant seismic velocities and densities in each, as shown in figure 5.

The example consists of simulating real seismic data by ray tracing in order to generate a synthetic data set. The data set is used in PSDM to generate a seismic depth section. Then, the new invention, ROAR, is used on the result from PSDM as described above. This makes it possible to check the accuracy of the method by comparing with the true reflection coefficients from the model in figure 5.

At the surface of the model in figure 5, a marine survey with 138 shot positions and 120 receivers are simulated. In a marine survey, the receivers are towed behind the shots. The distance between the shots are 25 m and the distance between the receivers are 25 m as well. The distance from a shot to the first receiver is 25 m while the distance from the shot to the last receiver (# 120) is 3000m. The distance between shot and receiver is generally termed the *offset*.

The seismic data from each of these 138 shots are simulated by ray modeling, as described in reference [9] and [10].

The total offset range from 25 m to 3000 m is divided into 10 sub intervals with offset from 25 to 300 m in the first interval, 325 to 600 m in the second interval etc. In figure 6, the result of PSDM of the synthetic data for the first offset interval is shown. The shape of the target reflector is clearly visible. In figure 7, the measured maximum amplitude along target reflector in the depth section in figure 6 is shown along with the true reflection coefficient for reflection angle equal to zero. The figure shows a poor correspondence between amplitudes from PSDM and the true reflection coefficient.

Using ROAR, the angle dependent reflection coefficient is approximated with a large degree of accuracy, as shown in figure 8. In this figure, the true reflection coefficient is plotted as solid lines and the estimates from ROAR with black dots. The upper of the solid curves corresponds to the reflection coefficient in the position $x=5$ km, while the lower one corresponds to the position $x=3$ km.

In figure 9, the estimated reflection coefficient for the lowermost offset interval (25 m to 300 m) is shown as black points along with the true reflection coefficient shown as a continuous curve. Notice that the estimated reflection coefficient is smoother than true reflection coefficient. This is caused by the limited resolution of the details in the RC by the ROAR method. A part of ROAR consists in a quantitative calculation of this resolution for all points along the target reflector by the weight functions. Two of the weight functions, W_1 and W_2 for two positions on the target reflector are shown at the top of figure 9. The weight functions show that the resolution is better in point C than in point D indicated in the figure.

The present invention is not restricted to that described above and shown in the drawings, but can also be modified and changed in a number of ways within the scope of the concept of the invention as stated in the following claims. For example, it can be considered using other methods for measuring the amplitudes or energy in the seismic cubes. One can also use other modeling methods than ray tracing for computing the synthetic traces.

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